

$$\sigma_{zm} = \left(\frac{E'_m}{Z} \right) \frac{\partial \phi_e}{\partial z} \quad (26)$$

$$\tau_{xzm} = \left(\frac{G_m}{F} \right) \frac{\partial \phi_e}{\partial x} \quad (27)$$

$$\tau_{zym} = \left(\frac{G_m}{F} \right) \frac{\partial \phi_e}{\partial y} \quad (28)$$

Furthermore, letting the analog device dimensions be (a, b, c) and letting the composite solid dimensions be (a_1, b_1, c_1) , all aspect ratio correspondences may be found by combinatorial division of the following expressions:

$$a_1 = Fa \quad (29)$$

$$b_1 = Fb \quad (30)$$

$$c_1 = Zc \quad (31)$$

e.g., $a_1/b_1 = a/b$ and $b_1/c_1 = (F/Z)b/c$. It is further convenient to let the analog device aspect ratios a/c and b/c be represented as

$$a/c = \alpha \quad (32)$$

and

$$b/c = \beta \quad (33)$$

Using Eqs. (29-33) one finds

$$a_1/c_1 = (F/Z)\alpha \quad (34)$$

$$b_1/c_1 = (F/Z)\beta \quad (35)$$

and

$$a_1/b_1 = \alpha/\beta \quad (36)$$

Thus in order to predict results over large material and geometry ranges for the composite solid (for a given damage configuration), one must be able to change α and β as easily as possible (once again note that $(F/Z)^2 = E'_m/G_m$). To this end the electrolyte depth can control b_1 , and a_1 can be controlled by constructing the analog device such that the width a can be easily adjusted (it may be more convenient to adjust c rather than a). It also appears that the easiest way to control F and Z is to vary the electrolyte resistivity. Other ingenious experimental setups may permit more efficient variation of other primitives.

Summary

It has been shown that

1) The composite solid/analog device *affine* equations are elastically and electrically *material independent*.

2) The analog experimental solutions for a given damaged state and given boundary conditions can yield the stress and displacement fields of the composite solid for a wide range of physical variables.

Acknowledgments

This work was supported by a joint National Aeronautics and Space Administration/U.S. Air Force Office of Scientific Research Grant NGL 33-018-003, with Dr. Michael Greenfield as Contract Monitor. Their continuing joint support is gratefully acknowledged. It is also a pleasure to thank Mrs. Anna Mae Harris for her most competent typing skills.

References

- ¹Batdorf, S. B., "Measurement of Local Stress Distributions in Damaged Composites using an Elastic Analogue," *Advances in Aerospace Structures and Materials-1982*, Proceedings of the ASME Structures and Materials Committee, Aerospace Div. Pub. AD-03, ASME, New York, 1982, pp. 71-74.

Errata: "An Alternating Method for Analysis of Surface-Flawed Aircraft Structural Components"

T. Nishioka and S. N. Atluri
Georgia Institute of Technology, Atlanta Georgia
[AIAAJ, 21, pp. 749-757 (1983)]

THE information contained in the footnote on page 749 of this article is incorrect. The footnote should read: "Presented as Paper 82-0742 at the AIAA/ASME/ASCE/AHS 23rd Structures, Structural Dynamics, and Materials Conference, New Orleans, La., May 10-12, 1982."

Received Sept. 25, 1983.